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Groundwater Extraction and

The Water Balance

By

George H. Hargreaves¹

ABSTRACT

Groundwater extraction and net use are related to groundwater depletion and the water balance. Potential evapotranspiration, actual crop or vegetative evapotranspiration, dependability of precipitation, moisture deficits and a moisture availability index are defined.

A method is presented for estimating potential evapotranspiration and crop evapotranspiration from a minimum of climatic data. For arid areas the only weather measurement required is temperature. Crop factors are presented for a wide variety of crops. A water balance study for an essentially closed basin in Nicaragua is described and used to illustrate the relationships proposed.

The economics of using groundwater extraction to prevent or alleviate drainage problems is discussed. Irrigation requirements are related to the economics of pumping water for irrigation.

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INTRODUCTION

A portion of the groundwater extracted from the area of withdrawal will be returned to the ground-water aquifer if the area of withdrawal corresponds to the area of water use. If net use of groundwater exceeds recharge there will be a lowering of the water table. It is frequently desirable to know in a general way what changes can be expected by various rates of use. A better understanding can be had of these changes providing evapotranspirational uses by crops and native vegetation can be estimated. Since in many areas only a minimum of data are available the procedure for estimation should be as simple as is practicable.

It sometimes becomes desirable that irrigation by groundwater extraction be combined with irrigation from rivers or reservoir storage in order to prevent or alleviate drainage problems. A better knowledge of net water use provides a criteria for planning and for the estimating of the amount of pumping required.

A knowledge of irrigation requirements is a necessary part of the economic analysis in feasibility studies for irrigation development whether from groundwater or surface supplies. This paper provides the basic procedures for accurately estimating net water requirements.

DEFINITION OF TERMS

<u>Actual Evapotranspiration</u>, ETA, or crop evapotranspiration is the water used by crops or vegetation including evaporation from moist soils and vegetation. It depends principally upon climate, rate and stage of crop growth and soil moisture availability.

Potential Evapotranspiration, ETP, is the amount of water transpired from an actively growing short green plant cover (usually grass) with a continuously adequate moisture supply. It includes evaporation from plants and from the soil surface. For this study values used are based upon short rye grass grown under conditions of low advection, deep rooted grasses at Coshocton, Ohio and grass mixtures having similar water requirements. It is dependent upon climate and can be estimated from climatic parameters.

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Dependable Precipitation, PD, is the precipitation at a specified probability of occurrence based upon a gamma distribution analysis. For irrigation development a seventy-five percent probability, or the rainfall that can be anticipated to be equalled or exceeded three years out of four based upon the available rainfall records, has been selected as a reasonable probability level for most agricultural conditions.

Moisture Deficit, ETDF, is the difference between potential evapotranspiration and the dependable precipitation. It is an index of irrigation needs and requirements.

Moisture Availability Index, MAI, is the ratio of dependable precipitation to the estimated potential evapotranspiration. For many crops, under uniform soil fertility and other conditions, production increases as a straight line function of MAI between values of MAI of 0.34 and 0.70 to 0.85. MAI is therefore proposed as a convenient index of moisture adequacy or deficiency from precipitation.

ESTIMATING POTENTIAL EVAPOTRANSPIRATION

The California State Department of Water Resources $(2)^2$ measured Class A pan evaporation from pans located in irrigated grass surrounds and grass and pasture evapotranspiration in various locations representing four distinct climatic zones. Grass and pasture evapotranspiration averaged about 0.80 times pan evaporation. This relationship was particularly well demonstrated by the data from the coastal fogbelt area. Based upon this study it is believed that for fairly large irrigated areas potential evapotranspiration, ETP, can be approximated from the equation

$$ETP = 0.80 \times EVPM$$
(1)

in which EVPM is the measured Class A pan evaporation from a pan located in a fairly large irrigated area. This relationship is also probably satisfactory for locations having fairly low sensible heat transfer as is the case for high humidities with low wind velocities. For highly advective conditions (hot dry windy weather), particularly with bare soil surrounds, the ratio of

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²Numerals in parentheses refer to corresponding items in the Appendix-References.

grass evapotranspiration from lysimeters to pan evaporation may be as low as 0.55 and possibly lower.

Blaney-Criddle, Thornthwaite and Hargreaves (5) have related potential evapotranspiration to day length and climatic factors. A methodology proposed by Christiansen (3) and since used and modified by various graduate students and technicians uses extraterrestrial radiation expressed as units of evaporation and coeffficients for the various weather elements. An equation for potential evapotranspiration, ETP, can be written that combines these concepts with an addition of a correction for latitude (sun angle). A monthly potential evapotranspiration factor, MF, is multiplied by temperature in degrees Fahrenheit, TMF, and relative humidity correction, CH, in order to obtain estimated values of ETP. The equation can be written

$$ETP = MF \times TMF \times CH$$
 (2)

in which

 $MF = C \times R \times DL/12 \times CLA$

where

C =	a constant depending upon the units of ETP
R =	extraterrestrial radiation expressed as equivalent evaporation by dividing the radiation (calories per square centimeter per day) by the heat of vaporization at the mean temperature in degrees centigrade, TM, and converting to appropriate units, usually inches or mm per month.
DL ·	Day length in hours (sunrise to sunset)
CLA :	= $0.17 \times (70 - ABLA)^{1/2}$ (2a) with a maximum value of 1.00
ABLA	absolute value of the latitude in degrees
CH	= 0.166 x $(100 - HM)^{1/2}$ (2b) with a maximum value of 1.00
HM	mean monthly 24-hour relative humidity in percent.

In arid climates (mean 24-hour relative humidity of 64 percent or less) the correction for humidity, CH, becomes 1.00 and can be omitted from equation 2. Values of MF depend only on latitude and can be published for all latitudes. The calculation of potential evapotranspiration for arid areas is therefore accomplished by multiplying a tabular value times mean temperature in degrees Fahrenheit. Values of MF, the monthly evapotranspiration factor, are given in inches per month and mm per month in Appendix III, Tables Al and A2. Computer equations for calculating monthly values, MF, of the potential evapotranspiration factor and daily values, DF, are also presented in Appendix III.

In order to demonstrate the validity of equation 2 a comparison was made between ETP and measured grass evapotranspiration, ETL, at various locations. These comparisons are shown for four locations, varying from latitude 56 degrees north to 38 degrees south, together with the climatic data in Appendix III.

CROP EVAPOTRANSPIRATION

A good summary of crop coefficients to be used with Class A pan evaporation from well standardized conditions is given by Middleton, Pruitt, Crandall and Jensen (7). The coefficients apply to full crop cover conditions and have been converted so as to apply to potential evapotranspiration, ETP. Crop evapotranspiration or actual evapotranspiration, ETA, is obtained from the equation

$$ETA = K \times ETP \tag{3}$$

in which K is a crop coefficient. Crop coefficients based upon those given by Middleton, et al. (7) are given in Table 1.

Crop	К		K
Apples, Delicious Alfalfa, Ranger (arid)	1.31	Potatoes, White Rose	1.21
Beans, Red Mexican	1.11	Potatoes, Neted Gem (late)	1.16
Soybeans Clover Ladino	1.11	Sorghum, NK 140	1.09
Corn (field)	1.15	Sorghum d.d. yellow Sooner Wheat. Marfed (spring)	0.96
Pear, Dark Perfection	0.96	Wheat, Omar (winter)	1.13
Peaches, Elberta (no cover)	1.25	Grapes, Concord (no cover)	0.86
cover)	1.00	Altalfa, DuPuits (humid) Rasberries. Payallup	1.16
Sugar Beets	1.13	Strawberries, Northeast	0.48

Table 1. Average Crop Coefficients to be Used for Full Crop Cover

All available sources of crop evapotranspiration data were used to provide a general summary of crop coefficients for both full crop cover conditions and for the growing season average. These coefficients are from the data available principally from agricultural experiment stations and various publications and are presented in Table 2.

Although timing of water availability has an important influence on crop growth and yields there is a general relationship between moisture adequacy and production. Scott (8) demonstrates essentially no change in production per unit of water applied between 45 and 75 percent of ETA. The moisture adequacy yield curve became approximately a straight line relationship within that range and yields per unit of water applied fell off with increasin'g adequacy up to 100 percent of the value ETP x K. The relationship beyond full adequacy is not given.

Various other crops demonstrate similar production functions with a maximum value of water in the production function occuring at about 70 to 85 percent of fully adequate application.

A WATER BALANCE STUDY

A water balance and irrigation requirements study was made in 1971 by the UNDP Groundwater Investigations in Nicaragua of the Chinandega-Leon drainage area. The area investigated is nearly a closed basin comprising 136,400 hectares. A land use inventory of all crops and vegetation groupings was available. Precipitation was measured at 23 locations. Groundwater outflow was estimated from water levels and well tests along the zone of outflow which is a very limited area.

Potential evapotranspiration was calculated from the weather data using monthly means. The crop coefficients used for full crop cover or full vegetative cover and full moisture availability are given in Table 3.

The crop coefficients were reduced during periods of less than full crop cover and during periods of less than full moisture availability. Dates of drying of vegetation were used to determine periods of moisture shortage.

Сгор	Average K for Full Crop Cover	Average Seasonal K
Field and oil crops including beans, castor beans, corn, cotton, flax, peanuts, potatoes, safflower, soybeans, sorghum, sugar beets, tomatoes, and wheat	1.15	. 90
Fruits, nuts and grapes Citrus fruits (oranges, lemons and grapefruit) Deciduous fruits (peaches, plums and walnuts) Deciduous fruits with cover crop Grapes	.75 .90 1.25 .75	.75 .70 1.00 .60
Hay, forage and cover crops		
Alfalfa Short grass Clover pasture Green Manure	1.35 1.00 1.15 1.10	1.00 1.00 .95
Sugar cane	1.25	1.00
Summer vegetables	1.15	.85

 Table 2. Crop Coefficients, K (for use with potential evapotranspiration

 ______ETP)

Crop or	Crop	Crop or	Crop
Vegetation	Coefficient	Vegetation	Coefficient
Sugar Cane Bananas Irrigated Pasture Vegetables Grain	1.25 1'.15 1.25 1.15 1.15	Cotton Improved Pastur Native Grass Forest	1.15 e 1.25 1.15 1.35

Table 3. Crop Coefficients for Full Cover and Full Moisture Adequacy - Chinandega-Leon Area, Nicaragua

The study included irrigation requirements and an estimate of the probable changes in water levels for various areas under irrigation. A summary was made for the area giving mean precipitation, vegetative consumptive use, changes in ground water storage, surface water outflow, unaccountable irrigation losses and ground water outflow. An estimate was made relative to the area that can be economically irrigated without adversely affecting the water balance.

EXTRACTING GROUNDWATER FOR DRAINAGE

A knowledge of crop evapotranspiration provides a useful criteria for evaluating the possibilities of controlling drainage problems or preventing a rise in water table elevations from creating drainage problems.

Pumping of groundwater has been planned as part of numerous surface irrigation projects. The irrigation planning and design for much of the east side in the Central Valley of California was based upon the assumption that 35 percent of the water used would be pumped from groundwater. This was to minimize future drainage problems.

The Modesto and Turlock irrigation districts in California formerly operated systems of open drains. They now use a system of wells to provide drainage as well as irrigation water resultin substantial profits from the irrigation water pumped. In the Salt River Valley of Arizona pumping about one third of the irrigation supply from groundwater solved the drainage problem.

Unfortunately not all drainage problems can be solved in this manner. Successful extraction of groundwater for drainage requires satisfactory water quality, a favorable salt balance and suitable aquifer conditions.

ECONOMIC CONSIDERATIONS

A fairly precise estimate of irrigation requirements is necessary in order to determine the desirable size of pump and motor and to make an economic analysis including capital and operating costs. Methods of preparing engineering costs estimates are given in various hand books. Less information, however, is available on the economics of under irrigating or over irrigating various crops.

Scott (8) made a study of the value of water used in producing sugar cane. If a factor is used to indicate available water used divided by the potential use by the cane expressed as a percentage, then the relationship of production to the percentage factor can be summarized as follows:

Percentage Factor	Tons of Cane Per Inc						
<u>(Use x 100/Max ETA)</u>	of Water Used						
45-75 percent	0.84						
80-90 percent	0.81						
95 percent	0.77						
100 percent	0.74						

The concept of a percentage factor is similar to the moisture availability index previously defined. Mirnizami, as cited by Hargreaves (4), related yields of dry farmed wheat to moisture levels. Regression equations were developed relating yield to MAI and to ETDF. Correlation coefficients for the unfertilized trials were in the range of 0.93 to 0.97. Although straight line relationships were demonstrated, the range in MAI was about 0.33 to 0.84. Production per unit of available moisture can be expected to fall off significantly with increasing moisture availability.

An attempt was made to obtain moisture availability and yield data from as many representative locations as possible. Scott (8) used lysimeter evapotranspiration for determining potential water use by sugar cane. Three locations were compared. Beckett and Huberty (1) presented yield data for alfalfa at Davis and Delhi in California as a function of irrigation water applied. Stewart and Hagan (9) reported corn yields at Davis as a function of season total water supply. Where necessary the moisture available from irrigation was corrected by adding moisture available from rainfall.

If Y is expressed as a ratio of actual yield to the maximum yield under the prevailing fertility level, cultural practices and other conditions and X is the ratio of moisture available to the amount for which the yield is a maximum, then Y will vary from 0 to 1.0 and X from 0 to 1.0 or more. Based upon the data cited above a generalized production function equation can be written

$$Y = 0.8X + 1.3X^2 - 1.1X^3$$
 (4)

Equation 4 results in a maximum increase in yield per increment increase in moisture at X = 0.394, Y = 0.450. The slope of the curve at this point is 1.31. The point where a unit increase in X produces a unit increase in Y (slope = 1.0) is X = 0.701, Y = 0.821. For values of X exceeding 1.02 Y decreases.

For sugar cane and alfalfa yield was maximum for a moisture adequacy or availbility approximately equal to the calculated values of ETP under the prevailing climatic conditions. Yield of corn was maximized at approximately 1.25 lysimeter evapotranspiration for corn (ETA) at the same location.

Although the slope of the production function may be influenced to some degree by fertility level, there was little scater in the relationship found from the data cited above. It is therefore proposed that equation 4 is adequate for most economic models for the purpose of determining an "economic" optimum level of moisture adequacy. This economic optimization would require use of all operational costs and the product value per unit of Y. It is of interest however to note that in equation 4 seventy percent of optimum moisture produces 82 percent of optimum yield.

Water extracted from aquifers is frequently relatively expensive. As full adequacy (crop actual evapotranspiration) is approached the production per unit of water applied falls off. A careful evaluation of crop evapotranspiration requirement is therefore necessary in evaluating maximum returns per unit of investment in groundwater development.

CONCLUSION

Fairly precise estimates of irrigation requirements and net water use are required in the planning and evaluation of ground water developments for irrigation. The solution of drainage problems and estimation of possible future depletion is greatly facilitated through improved estimates of potential evapotranspiration. Methodology is presented for estimating potential evapotranspiration from a minimum of weather data for a wide range of climatic conditions. For most climates the only weather data required are mean temperature and mean humidity. For arid climates only temperature data are required.

Crop coefficients for use with potential evapotranspiration are based upon available sources from various parts of the world. The coefficients presented appear satisfactory for use in connection with prevailing cultural practices.

Under favorable conditions pumping from groundwater for irrigation provides an economically feasible method of furnishing drainage for gravity irrigation projects.

Since production per unit of water applied falls off above about 70 to 85 percent of full moisture adequacy, a good knowledge of crop water requirements is necessary for the economic evaluation of projects for the use of ground-water extraction for irrigation.

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APPENDIX II - NOTATION

Notations used in the text and in Appendix III are defined as follows: ABLA = absolute value of the latitude in degrees C = a constant in the evapotranspiration equation CH = dimensionless coefficient for mean 24-hour relative humidity CLA = dimensionless latitude correction DEC = declination (angle of the sun) DER = declination in radians DETP = ETL - ETPDF = daily evapotranspiration factor DL = day length in hours (sunrise to sunset) DM = number of days in the month ETA = actual crop evapotranspiration ETDF = moisture deficit or evapotranspiration deficit ETIN = potential evapotranspiration in inches (monthly) ETL = grass evapotranspiration in mm from lysimeter measurements ETP = potential evapotranspiration in mm (monthly) ETPD = potential evapotranspiration (daily values) ES = mean monthly distance of the sun to the earth divided by the mean solar distance EVPM = measured Class A pan evaporation F = evapotranspiration factor in Tables A1 and A2 (MF) $FTMF = F \times TMF \text{ or } MF \times TMF$ HM = mean 24-hour relative humidity for the period K = crop coefficient for estimating ETA LD = degrees of latitude LDM = minutes of latitude MAI = moisture availability index (MAI = PD/ETP) MF = monthly evapotranspiration factor MO = month of the yearPD = dependable precipitation at 75 percent probability (that equalled or exceeded three years out of four) R = extraterrestrial radiation expressed as equivalent evaporation

- RH = mean 24-hour relative humidity (HM)
- RLD = extraterrestrial radiation in Langleys per day
- RMD = R in mm per day at TM
- RMM = R in mm per month at TM
- TM = mean temperature in degrees centigrade
- TMF = mean temperature in degrees Fahrenheit
 - X = ratio of moisture availability to the amount for which yield is a maximum
- XLR = latitude in radians
 - Y ratio of actual yield to maximum yield under prevailing conditions and practices.

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APPENDIX III - COMPUTER EQUATIONS, ETP-ETL COMPARISONS AND ETP FACTORS

Computer Programs

Parts of computer programs are presented giving the data required and the equations for calculating day length, extraterrestrial radiation and potential evapotranspiration. Equations are given for daily and monthly values. The symbols used are explained in Appendix II.

Computer Comparisons of ETP with ETL

Climatic data and comparisons of ETP with ETL are presented. Data used are from four locations where evapotranspiration measurements were available for all twelve months of the year. The locations are: Davis, California; Coshocton, Ohio; Copenhagen, Denmark and Aspendale, Australia. An explanation of the column headings is given in Appendix II.

Potential Evapotranspiration Factor, F, or MF

Tables A1 and A2 give values of a potential evapotranspiration factor in inches per month and in mm per month. This factor, F, is used to calculate ETP by multiplying F times TMF (mean temperature) and where appropriate, applying a correction for relative humidity. For arid climates (mean 24-hour relative humidity of 64 percent or less) a correction for relative humidity is not required.

```
DATA USED FOR CALCULATION OF DAY LENGTH AND RADIATION
   DATA (DH(H), H=1+12)/31.+28.+31.+30.+31.+30.+31.+30.+31.+30.+31.+30.+
 131./
  DATA (DEC(M),M=1+12)/-20.949,-13.553,-2.683,9.207,18.606,23.016,21
 $.195,13.523,2.289,-9.565,-18.854,-23.040/
  DATA (ES(H),M=1,12)/.97104,.98136,.99653,1.01313,1.02625,1.03241,1
 $.02987+1.01916+1.00347+.98693+.97369+.96812/
   CALCULATION OF DAY LENGTH (DL) AND RADIATION (RMM)
   XLR=(FLOAT(LD)+FLOAT(LDM)/60.)/57.2958
   DER=DEC(M)/57.2958
   Z=-TAN(XLR)+TAN(DER)
   IF(2)7,8,7
 7 OM=ATAN(SQRT(1.0-Z*Z)/ABS(Z))
   GO TO 9
 8 0M=1.5708
 9 DL=0M/C.1309
   IF(7)12,13,13
12 DL=24.-DL
13 RLD=120.*(DL*SIN(XLR)*SIN(DER)+7.6394*COS(XLR)*COS(DER)*SIN(OM)/ES
  1(M))
   RMD=10.+RLD/(595.9-C.55+TM(N))
   RMM=RMD+DM(M)
   CALCULATION OF MONTHLY ETP
          ABLA=ABS(FLOAT(LD)+FLOAT(LDH)/60.)
   CLA=.17+SQRT(70.-ABLA)
   IF(CLA.GT.1.0C) CLA=1.00
   CH=.166+SQRT(100.-HM(H))
   IF(CH.GT. 1.00)CH=1.00
   MF=RMM+DL/12.+CL A+.COC190
   TMF=32.+1.8+TM(M)
   ETP=HF+TMF+25.4+CH
```

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```
CALCULATION OF DAILY ETP
 2 CONTINUE
   D=0.
   DO 90 M=1,12
   ND=DM(M)
   DO 80 K=1.ND
   NDA(K)=K
   D=D+1.
   Y=COS(0.0172142*(D+192.))
   DER=0.40876+Y
   DECL=57.2958+DER
   ES=1.00028+.03269+Y
   Z=-TAN(XLR) + TAN(DER)
   IF(Z) 44,43,42
42 OM=ATAN(SQRT(1.0-Z*Z)/ABS(Z))
   DL=0M/0.1309
   GO TO 45
43 OM=1.5708
   DL=12.
   GO TO 45
44 OM=ATAN(SGRT(1.0-Z+Z)/ABS(Z))
   DL=24 - (OM/0.13C9)
45 CONTINUE
   RLD=120.*(DL+SIN(XLR)+SIN(DER)+7.639+COS(XLR)+COS(DER)+SIN(OM))/ES
   PHD=1C.+RLD/(595.0-.55+TM)
   DF=RMD+DL/12.+CL A+.000190+25.4
   ETPD(K+M)=DF+TMF+CH
80 CONTINUE
90 CONTINUE
```

19	360 `	DAI	VIS CAL	IFORNIA	L	AT 38 32	2 LONG	121 46	ELEY	18		
MO	TM	TMF	RH	Сн	RMM	MF	FTHF	ETL	ETP	ETIN	DETP	RE
1	7.4	45.	75.	•83	205.	•758	34.	29.	29.	1.14	0.	1.0
2	9.2	49.	64.	1.00	241.	•974	47.	63.	47.	2.48	16.	1.3
3	12.8	55.	68.	•94	356.	1.602	88.	87.	83.	3.43	4.	1.0
4	13.9	57.	66.	•97	432.	2.150	123.	120.	119.	4.72	1.	1.0
5	17.0	63.	55 .	• 98	510.	2.753	172.	158.	169.	5.22	11.	•9
5	23.3	74.	57.	1.00	523.	2.934	217.	221.	217.	8.70	4.	1.0
1	24.5	76.	57.	1.00	530.	2.925	223.	214.	223.	8.43	-9.	•9
8	20.5	69.	60.	1.00	479.	2.473	170.	166.	170.	6.54	-4.	•9
9	20.4	59 .	57.	1.00	385.	1.807	124.	132.	124.	5.20	8.	1.0
10	15.8	62.	54.	1.00	302.	1.272	79.	94.	79.	3.70	15.	1.1
,11	- 10-9	52.	73.	• 86	216.	-821	42.	39.	37.	1.54	2.	1.0
12	7•2	45.	77.	•80	189.	•674	30.	27.	24 •	1.06	3.	1.1
AVE	15.3	60.	64.	• 95	364.	1.762	113.	112.	110.	4.43	2.	1.0
	•						-					
15	YR AV	COS	HOCTON	OHIO	LA	T 40 22	LONG	81 48	ELEV	3 60	. .	-
15 Mo	YR AV TM	COS TMF	HOCTON RH	оніо Сн	LA Rmm	T 40 22 MF	LONG FTMF	81 48 Etl	ELEV Etp	360 Etin	DETP	RE
15 Mo 1	YR AV Th -2.8	COS TMF 27.	HOCTON RH 75.	0HI0 Ch •83	LA RMM 189.	T 40 22 MF •666	LONG FTMF 18.	81 48 Etl 17.	ELEV ETP 15.	360 Etin •67	DETP	RE
15 MO 1 2	YR AV Tm -2.8 -1.6	COS TMF 27. 29.	5HOCTON RH 75. 72.	0HI0 Ch .83 .88	LA RMM 189. 227.	T 40 22 MF •666 •881	LONG FTMF 18. 25.	81 48 ETL 17. 27.	ELEV ETP 15. 23.	360 ETIN •67 1•06	DETP 2. 4.	RE 1•1 1•2
15 MO 1 2 3	YR AV Tm -2.8 -1.6 2.5	COS TMF 27. 29. 37.	5HOCTON RH 75. 72. 71.	0HI0 CH -83 -88 -88	LA RMM 189. 227. 343.	T 40 22 MF .666 .881 1.491	LONG FTMF 18. 26. 55.	81 48 ETL 17. 27. 42.	ELEV ETP 15. 23. 49.	360 ETIN .67 1.06 1.65	DETP 2. 4. -7.	RE 1.1 1.2 .8
15 MO 1 2 3 4	YR AV Th -2.8 -1.6 2.6 9.6	COS TMF 27. 29. 37. 49.	RHOCTON RH 75. 72. 71. 68.	OHIO CH .83 .88 .89 .94	LA RMM 189. 227. 343. 424.	T 40 22 MF •666 •881 1•491 2•059	LONG FTMF 18. 26. 55. 101.	81 48 ETL 17. 27. 42. 80.	ELEV ETP 15. 23. 49. 95.	360 ETIN •67 1•06 1•65 3•15	DETP 2. 4. -7.	RE 1.1 1.2 .8
15 MO 1 2 3 4 5	YR AV TM -2.8 -1.6 2.6 9.6 16.0	COS TMF 27. 29. 37. 49. 61.	RH 75. 72. 71. 68. 71.	OHIO CH .83 .88 .89 .94 .89	LA RMM 189. 227. 343. 424. 508.	T 40 22 MF •666 •881 1.491 2.059 2.687	LONG FTMF 18. 26. 55. 101. 163.	81 48 ETL 17. 27. 42. 80. 153.	ELEV ETP 15. 23. 49. 95. 146.	3 60 ETIN •67 1•06 1•65 3•15 6•02	DETP 2. 4. -7. -15. 7.	RE 1•1 1•2 •8 •8
15 MO 1 2 3 4 5 5	YR AV TM -2.8 -1.6 2.6 9.6 16-0 20.0	COS TMF 27. 29. 37. 49. 61. 58.	5HOCTON RH 75. 72. 71. 68. 71. 75.	0HIO CH - 83 - 88 - 89 - 94 - 89 - 83	LA RMM 189. 227. 343. 424. 508. 522.	T 40 22 MF .666 .881 1.491 2.059 2.687 2.877	LONG FTHF 18. 26. 55. 101. 163. 196.	81 48 ETL 17. 27. 42. 80. 153. 170.	ELEV ETP 15. 23. 49. 95. 145. 162.	3 60 ETIN •67 1•06 1•65 3•15 6•02 6•69	DETP 2. 4. -7. -15. 7. 8.	RE 1.1 1.2 .8 .8 1.0
15 MO 1 2 3 4 5 6 7	YR AV TM -2.8 -1.6 2.6 9.6 16.0 20.0 22.5	COS TMF 27. 29. 37. 49. 61. 61. 68. 73.	RH 75. 72. 71. 68. 71. 75. 73.	0HIO CH -83 -88 -89 -94 -89 -83 -83 -86	LA RMM 189. 227. 343. 424. 508. 522. 528.	T 40 22 MF .6666 .881 1.491 2.059 2.687 2.877 2.864	LONG FTMF 18. 26. 55. 101. 163. 196. 208.	81 48 ETL 17. 27. 42. 80. 153. 170. 173.	ELEV ETP 15. 23. 49. 95. 146. 162. 180.	3 60 ETIN •67 1.06 1.65 3.15 6.02 6.69 6.81	DETP 2. 4. -7. -15. 7. 8. -7.	RE 1.1 1.2 .8 .8 1.0 1.0
15 MO 1 2 3 4 5 6 7 8	YR AV TM -2.8 -1.6 2.6 9.6 16.0 20.0 22.6 22.0	COS TMF 27. 29. 37. 49. 61. 68. 73. 72.	5HOCTON RH 75. 72. 71. 68. 71. 75. 73. 74.	OHIO CH -83 -88 -89 -94 -89 -83 -83 -86 -85	LA RMM 189. 227. 343. 424. 508. 522. 528. 475.	T 40 22 MF .666 .881 1.491 2.059 2.687 2.877 2.864 2.399	LONG FTMF 18. 26. 55. 101. 163. 196. 208. 172.	81 48 ETL 17. 27. 42. 80. 153. 170. 173. 149.	ELEV ETP 15. 23. 49. 95. 145. 162. 180. 145.	3 60 ETIN •67 1.06 1.65 3.15 6.02 6.69 6.81 5.87	DETP 2. 4. -7. -15. 7. 8. -7. 4.	RE 1.1 1.2 .8 1.0 1.0 1.0 1.0
15 MO 1 2 3 4 5 6 7 8 9	YR AV TM -2.8 -1.6 2.6 9.6 16.0 20.0 22.6 22.0 18.2	COS TMF 27. 29. 37. 49. 61. 68. 73. 72. 65.	RH 75. 72. 71. 68. 71. 75. 73. 74. 74.	OHIO CH -83 -88 -89 -94 -89 -83 -85 -85 -85	LA RMM 189. 227. 343. 424. 508. 528. 528. 475. 375.	T 40 22 MF .666 .881 1.491 2.059 2.687 2.877 2.864 2.399 1.713	LONG FTMF 18. 26. 55. 101. 163. 196. 208. 172. 111.	81 48 ETL 17. 27. 42. 80. 153. 170. 173. 149. 103.	ELEV ETP 15. 23. 49. 95. 145. 162. 180. 145. 94.	3 60 ETIN •67 1•06 1•65 3•15 6•02 6•69 6•81 5•87 4•06	DETP 2. 4. -7. -15. 7. 8. -7. 4. 9.	RE 1.1 1.2 .8 1.0 1.0 1.0 1.0 1.0
15 MO 1 2 3 4 5 6 7 8 9 10	YR AV TM -2.8 -1.6 2.6 9.6 16.0 20.0 22.5 22.0 18.2 12.1	COS TMF 27. 29. 37. 49. 61. 68. 73. 72. 65. 54.	RH 75. 72. 71. 68. 71. 75. 73. 74. 74. 71.	OHIO CH .83 .88 .89 .94 .89 .83 .85 .85 .85 .85 .89	LA RMM 189. 227. 343. 424. 508. 528. 528. 475. 375. 288.	T 40 22 MF .666 .881 1.491 2.059 2.687 2.877 2.864 2.399 1.713 1.170	LONG FTMF 18. 26. 55. 101. 163. 196. 208. 172. 111. 63.	81 48 ETL 17. 27. 42. 80. 153. 153. 170. 173. 149. 103. 65.	ELEV ETP 15. 23. 49. 95. 146. 162. 180. 145. 94. 56.	3 60 ETIN •67 1•06 1•65 3•15 6•02 6•69 6•81 5•87 4•06 2•56	DETP 2. 4. -7. -15. 7. 8. -7. 4. 9. 9.	RE 1.1 1.2 .8 1.0 1.0 1.0 .9 1.0 1.1 1.1
15 MO 1 2 3 4 5 6 7 8 9 10 11	YR AV TM -2.8 -1.6 2.6 9.6 16.0 20.0 22.6 22.0 18.2 12.1 4.5	COS TMF 27. 29. 37. 49. 61. 68. 73. 72. 65. 54. 40.	RH 75. 72. 71. 68. 71. 75. 73. 74. 74. 71. 74. 74.	OHIO CH .83 .88 .89 .94 .89 .83 .85 .85 .85 .85 .89 .85	LA RMM 189. 227. 343. 424. 508. 522. 528. 475. 375. 288. 201.	T 40 22 MF •666 •881 1•491 2•059 2•687 2•877 2•864 2•399 1•713 1•170 •730	LONG FTMF 18. 26. 55. 101. 163. 196. 208. 172. 111. 63. 29.	81 48 ETL 17. 27. 42. 80. 153. 153. 170. 173. 149. 103. 65. 25.	ELEV ETP 15. 23. 49. 95. 146. 162. 180. 145. 94. 56. 25.	3 60 ETIN •67 1•06 1•65 3•15 6•02 6•69 6•81 5•87 4•06 2•56 •98	DETP 2. 4. -7. -15. 7. 8. -7. 4. 9. 9. 0.	RE 1.1 1.2 .8 .8 1.0 1.0 1.0 1.0 1.0 1.1 1.1
15 MO 1 2 3 4 5 6 7 8 9 10 11 12	YR AV TM -2.8 -1.6 2.6 9.6 16.0 20.0 22.6 22.0 18.2 12.1 4.5 -1.8	COS TMF 27. 29. 37. 49. 61. 68. 73. 72. 65. 54. 40. 29.	RH 75. 72. 71. 68. 71. 75. 73. 74. 74. 74. 74. 79.	OHIO CH .83 .88 .89 .94 .89 .83 .86 .85 .85 .85 .89 .85 .76	LA RMM 189. 227. 343. 424. 508. 522. 528. 475. 375. 288. 201. 172.	MF .666 .881 1.491 2.059 2.687 2.877 2.864 2.399 1.713 1.170 .730 .587	LONG FTMF 18. 26. 55. 101. 163. 196. 208. 172. 111. 63. 29. 17.	81 48 ETL 17. 27. 42. 80. 153. 170. 173. 149. 103. 65. 25. 16.	ELEV ETP 15. 23. 49. 95. 146. 162. 180. 145. 94. 56. 25. 13.	3 60 ETIN .67 1.06 1.65 3.15 6.02 6.69 6.81 5.87 4.06 2.56 .98 .63	DETP 2. 4. -7. -15. 7. 8. -7. 4. 9. 9. 0. 3.	RE 1.1 1.2 .8 1.0 1.0 1.0 1.0 1.1 1.1 1.2 1.2 .9 1.1 1.1 1.2 1.2 .8 .8 1.0 1.2 .8 .8 1.0 1.2 .8 .8 .8 .8 .8 .8 .9 1.0 .0 .9 1.1 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0

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-18-

19	871	COI	PENHAGEN	DENMA	RK LA	AT 55 41	LONG	12 33	ELEV	10		
MO	тм	THF	RH	Сн	RMH	ME	FTNE	ET1	570	CTTN	0 570	057
1	-•3	31.	91.	•50	73.	-140	4		215	L[1N 1C	UEIP	REI
2	1.5	35.	83.	•68	122.	•293	10-	9_	7 .	•10	2.	1.82
3	•2	32.	82.	•70	241.	•716	23-	12.	15.	• 33 . h7	 D	- 1 - 29
4	5.8	42.	72.	.88	357.	1.278	54.	34.	48.	1.34		• / 4
5	11.5	53.	70.	• 91	477.	1.965	104-	86.	94.	7.79	-140	•/1
6	13.5	56.	77.	•80	512.	2.268	128-	77-	102.	3.07	-25	•91
7	16.5	62.	79.	• 76	509.	2.187	135.	102-	107.	5-05	-23.	• / 6
8	16.5	62.	77.	-80	421.	1.606	99.	92.	79.	7 62	-1-	• 9 9
9	12.0	54.	79.	•75	287.	•923	49.	43.	7.9	3.02	13+	1.1/
10	9.4	49.	78.	.78	174.	.455	22.	28.	17.	1 10	20 71	
11	4.5	40.	82.	.70	87.	-180	7.	9.	5.	1010		1.62
12	5.1	41.	83.	•68	57.	.101	4.	8.	3.	• 35	4 e E	1.11
									Je	• 51	3.	2.80
AVE	8•C	46.	79.	•75	276.	1.009	53.	42.	43.	1.65	-1.	1.31
19	61	ASP	PENDALE #	USTRAL	IA LA	T -38 C	L ON G	145 0	ELEV	20	•	
19 Mo	61 TM	ASP THF	PENDALE # RH	USTRAL CH	.IA LA Rmm	T -38 C MF	L ON G Ft mf	145 O Etl	ELEV Etp	20 Fttn	Neto	DET
19 Mo 1	61 TM 23•8	ASP ThF 75.	PENDALE # RH 57.	CH CH	IA LA RMM 560.	T -38 C MF 3.101	LONG FTHF 232.	145 0 ETL 254.	ELEV ETP 232	20 Etin 10-00	DETP	RET
19 Mo 1 2	61 Th 23•8 22•3	ASP THF 75. 72.	PENDALE # RH 57. 52.	CH 1.00 1.00	IA LA RMM 56C. 451.	T -38 C MF 3.101 2.346	L ON G FT MF 232. 169.	145 0 ETL 254. 183.	ELEV ETP 232. 169.	20 ETIN 10.00 7.20	DETP 22.	RET 1.09
19 MO 1 2 3	61 TH 23.8 22.3 19.6	ASP THF 75. 72. 67.	PENDALE # RH 57. 52. 66.	CH 1.00 1.00 .97	IA LA RMM 56C. 451. 406.	T -38 C MF 3.101 2.345 1.928	L ONG FT MF 232. 169. 130.	145 0 ETL 254. 183. 132.	ELEV ETP 232. 169. 126.	20 ETIN 10.00 7.20 5.20	DETP 22. 14.	RET 1.09 1.08
19 Mo 1 2 3 4	51 TH 23.8 22.3 19.6 17.8	ASP THF 75. 72. 67. 64.	PENDALE # RH 57. 52. 66. 70.	CH CH 1.00 .97 .91	IA LA RMM 56C. 451. 406. 291.	T -38 C MF 3.101 2.345 1.928 1.243	L ONG FTHF 232. 169. 130. 80.	145 0 ETL 254. 183. 132. 76.	ELEV ETP 232. 169. 126. 72.	20 ETIN 10.00 7.20 5.20 2.99	DETP 22. 14. 6.	RET 1.09 1.08 1.05
19 Mo 1 2 3 4 5	51 TH 23.8 22.3 19.6 17.8 13.1	ASP THF 75. 72. 67. 64. 56.	PENDALE # RH 57. 52. 66. 70. 80.	CH CH 1.00 .97 .91 .74	IA LA RMM 56C. 451. 406. 291. 218.	T -38 C MF 3.101 2.346 1.928 1.243 .842	L ONG FTHF 232. 169. 130. 80. 47.	145 0 ETL 254. 183. 132. 76. 40.	ELEV ETP 232. 169. 126. 72.	20 ETIN 10.00 7.20 5.20 2.99 1.57	DETP 22. 14. 5. 4.	RET 1.09 1.08 1.05 1.05
19 M0 1 2 3 4 5 6	51 TH 23.8 22.3 19.6 17.8 13.1 12.0	ASP THF 75. 72. 67. 64. 56. -54.	PENDALE # RH 57. 52. 66. 70. 80. 80.	CH 1.00 1.00 .97 .91 .74 .74	IA LA RMM 56C. 451. 406. 291. 218. 175.	T -38 C MF 3.101 2.346 1.928 1.243 .842 .638	L ONG FTHF 232. 169. 130. 80. 47. 34.	145 0 ETL 254. 183. 132. 76. 40. 29.	ELEV ETP 232. 169. 126. 72. 35.	20 ETIN 10.00 7.20 5.20 2.99 1.57 1.14	DETP 22. 14. 6. 4. 5.	RET 1.09 1.08 1.05 1.05 1.15
190 MO 1 2 3 4 5 6 7	51 TH 23.8 22.3 19.6 17.8 13.1 12.0 10.1	ASP THF 75. 72. 67. 64. 56. -54. 50.	PENDALE # RH 57. 52. 66. 70. 80. 80. 80.	CH 1.00 1.00 .97 .91 .74 .74 .74	IA LA RMM 56C. 451. 406. 291. 218. 175. 196.	T -38 C MF 3.101 2.346 1.928 1.243 .842 .638 .731	L ONG FTHF 232. 169. 130. 80. 47. 34. 37.	145 0 ETL 254. 183. 132. 76. 40. 29. 28.	ELEV ETP 232. 169. 126. 72. 35. 25. 27.	20 ETIN 10.00 7.20 5.20 2.99 1.57 1.14	DETP 22. 14. 6. 4. 5. 4.	RET 1.09 1.08 1.05 1.05 1.15 1.14
190 M0 1 2 3 4 5 6 7 8	51 TH 23.8 22.3 19.6 17.8 13.1 12.0 10.1 11.2	ASP THF 75. 72. 67. 64. 56. -54. 50. 52.	PENDALE # RH 57. 52. 66. 70. 80. 80. 80. 80. 80. 80. 83.	CH 1.00 1.00 .97 .91 .74 .74 .74 .74 .68	IA LA RMM 56C. 451. 406. 291. 218. 175. 196. 262.	T -38 C MF 3.101 2.346 1.928 1.243 .842 .638 .731 1.069	L ONG FTHF 232. 169. 130. 80. 47. 34. 37. 56.	145 0 ETL 254. 183. 132. 76. 40. 29. 28. 38.	ELEV ETP 232. 169. 126. 72. 35. 25. 27. 38.	20 ETIN 10.00 7.20 5.20 2.99 1.57 1.14 1.10	DETP 22. 14. 6. 4. 5. 4. 1.	RET 1.09 1.08 1.05 1.05 1.15 1.14 1.03
19 MO 1 2 3 4 5 5 7 8 9	51 TH 23.8 22.3 19.6 17.8 13.1 12.0 10.1 11.2 13.8	ASP THF 75. 72. 67. 64. 56. -54. 50. 52. 57.	PENDALE # RH 57. 52. 66. 70. 80. 80. 80. 80. 80. 80. 80. 80. 80. 8	CH 1.00 1.00 .97 .91 .74 .74 .74 .68 .92	IA LA RMM 56C. 451. 406. 291. 218. 175. 196. 262. 349.	T -38 C MF 3.101 2.346 1.928 1.243 .842 .638 .731 1.069 1.587	L ONG FTHF 232. 169. 130. 80. 47. 34. 37. 56. 90.	145 0 ETL 254. 183. 132. 76. 40. 29. 28. 38. 77.	ELEV ETP 232. 169. 126. 72. 35. 25. 27. 38. 83.	20 ETIN 10.00 7.20 5.20 2.99 1.57 1.14 1.10 1.50 3.03	DETP 22. 14. 6. 4. 5. 4. 1. -0.	RET 1.09 1.08 1.05 1.05 1.15 1.14 1.03 1.00
19 MO 1 2 3 4 5 6 7 8 9 10	51 TH 23.8 22.3 19.6 17.8 13.1 12.0 10.1 11.2 13.8 17.2	ASP THF 75. 72. 67. 64. 56. 56. 50. 52. 57. 63.	PENDALE # RH 57. 52. 66. 70. 80. 80. 80. 80. 83. 69. 62.	CH 1.00 1.00 .97 .91 .74 .74 .74 .68 .92 1.00	IA LA RMM 56C. 451. 405. 291. 218. 175. 196. 262. 349. 464.	T -38 C MF 3.101 2.346 1.928 1.243 .842 .638 .731 1.069 1.587 2.333	L ONG FTHF 232. 169. 130. 80. 47. 34. 37. 56. 90. 147.	145 0 ETL 254. 183. 132. 76. 40. 29. 28. 38. 77. 134.	ELEV ETP 232. 169. 126. 72. 35. 25. 27. 38. 83. 147.	20 ETIN 10.00 7.20 5.20 2.99 1.57 1.14 1.10 1.50 3.03 5.28	DETP 22. 14. 6. 4. 5. 4. 1. -0. -6.	RET 1.09 1.08 1.05 1.05 1.15 1.14 1.03 1.00 .92
19 MO 1 2 3 4 5 6 7 8 9 10 11	51 TH 23.8 22.3 19.6 17.8 13.1 12.0 10.1 11.2 13.8 17.2 18.7	ASP THF 75. 72. 67. 64. 56. 55. 50. 52. 57. 63. 65.	PENDALE # RH 57. 52. 66. 70. 80. 80. 80. 80. 83. 69. 69. 59.	CH 1.00 1.00 .97 .91 .74 .74 .74 .68 .92 1.00 1.00	IA LA RMM 56C. 451. 4C6. 291. 218. 175. 196. 262. 349. 464. 523.	T -38 C MF 3.101 2.346 1.928 1.243 .842 .638 .731 1.069 1.587 2.333 2.846	L ONG FTHF 232. 169. 130. 80. 47. 34. 37. 56. 90. 147. 187.	145 0 ETL 254. 183. 132. 76. 40. 29. 28. 38. 77. 134. 173.	ELEV ETP 232. 169. 126. 72. 35. 25. 27. 38. 83. 147. 187.	20 ETIN 10.00 7.20 5.20 2.99 1.57 1.14 1.10 1.50 3.03 5.28 5.81	DETP 22. 14. 6. 4. 5. 4. 1. -0. -13. -13.	RET 1.09 1.08 1.05 1.05 1.15 1.14 1.03 1.00 .92 .91
19 MO 1 2 3 4 5 5 7 8 9 10 11 12	51 TH 23.8 22.3 19.6 17.8 13.1 12.0 10.1 11.2 13.8 17.2 18.7 19.7	ASP THF 75. 72. 67. 64. 56. 55. 50. 52. 57. 63. 65. 67.	PENDALE # RH 57. 52. 66. 70. 80. 80. 80. 80. 83. 69. 62. 59. 58.	CH 1.00 1.00 .97 .91 .74 .74 .68 .92 1.00 1.00 1.00	IA LA RMM 56C. 451. 406. 291. 218. 175. 196. 262. 349. 464. 523. 574.	T -38 C MF 3.101 2.346 1.928 1.243 .842 .638 .731 1.069 1.587 2.333 2.846 3.238	L ONG FTHF 232. 169. 130. 80. 47. 34. 37. 56. 90. 147. 187. 218.	145 0 ETL 254. 183. 132. 76. 40. 29. 28. 38. 77. 134. 173. 190.	ELEV ETP 232. 169. 126. 72. 35. 25. 27. 38. 83. 147. 187. 218.	20 ETIN 10.00 7.20 5.20 2.99 1.57 1.14 1.10 1.50 3.03 5.28 6.81 7.48	DETP 22. 14. 6. 4. 5. 4. 1. -0. -6. -13. -14. -28.	RET 1.09 1.08 1.05 1.05 1.15 1.14 1.03 1.00 .92 .91 .93

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NOR1 LAT	TIE JAN	FEB	MAR	APR	HONTH May	JUN	JUL	AUG	SEP	001	NOV	DEC
		007	071	041	. 067	- 0.80	-076	-053	-078	.012	.004	•C01
60	•00Z	•007	.022	-043	4007 4070	-082	.078	.055	.070	.013	.004	.002
27	•UU 3	.000	.024	.046	4072	.085	.081	.058	.032	.015	•005	.002
20 67	.004	-010	.026	048	.075	.087	.093	-060	•C34	.016	-006	•003
56	.005	.011	.0Z 8	.050	.077	.089	.086	•063	• D3 G	.018	•007	.004
55	.0D£	.013	•030	.053	.080	.091	•088	.065	.038	.019	.008	.005
54	.007	.014	.032	•055	• D8 Z	•093	•090	•1167	•040	.021	• 009	•005
53	.008	.015	.034	.057	•084	.095	.092	•070	•042	.022	•010	•UUti
52	•009	.017	.036	• 059	.086	• 097	•094	•07Z	• 64 4	+024	+011	• UU /
51	.011	.018	.038	•061	.058	•033	•1120	•0/4	4040	9UK 0	0113	
50	.012	.019	.040	.063	.090	.100	.098	.076	.048	.028	.014	-010
49	•013	•021	.042	.065	•092	.10Z	•100	.078	•050	•U29	•015	4ULA - 1119
48	.014	•022	.044	• 067	.094	.103	•101	-080	+U3 <i>2</i>	.033	-018	-013
47	•016	+024	.096	.069	•036	-105	-103	-082	-056	.035	.020	.015
46	•017	•026	.048	• 0 / 1	•097	•100	•105	-004				
45	.019	.027	.050	.073	• 099	.108	•105	•086	•058	•037	•021	.016
99	.021	•029	.052	.075	.101	.109	.108	.088	.000	-039	+UZ3 020	1.019
43	• 02 2	.031	.054	.077	-102	.110	•109	-050	+UUZ	.041	-025	.021
42	• 024	•032	.056	•079	•104	.113	-112	•093	.066	.045	.028	.022
41	• 02 6	+034	.030									
40	.027	•036	.060	.083	•107	•114	-113	•095	•058	+U47	-012	+024
39	• C2 9	•038	•063-	.084	.108	•115	4114	-027	.072	-051	-032	.028
38	+031	•040	•065	• U05	.119	-117	-115	-100	.074	.053	.036	.030
37	•033	.044	.069	.089	.112	•117	-117	.101	.076	.056	.038	•032
				001			.118	.107	.077	-057	-039	•033
35	•037	.045	.070	• U 91	+112	-117	-117	-102	-078	.059	.041	.035
39	•039	040	-073	. 091	.111	-116	.116	.102	.079	.060	.042	.037
33	-042	.040	.074	.091	.111	.115	.116	.102	.080	•061	+044	•038
31	.043	.050	.074	.092	.110	.114	•115	•102	•080	.063	•045	•040
10	.045	-052	.075	.092	.110	.113	.114	•102	.081	.064	.047	•C41
29	.046	.053	.076	.092	.109	.112	•113	•102	•082	•065	•048	•043
28	.048	.054	.077	.092	.109	•111	•112	.102	.082	.066	•050	+ 044
27	+049	•055	.078	•093	•108	.110	•112	•102	.083	.067	•051	•046
26	.051	•056	.079	• 093	•108	•109	•111	•101	•083	•069	•052	-040
25	.052	.058	.080	• 0 9 3	• 107	.108	•110	.101	.084	.070	+054	.049
24	-054	.059	.081	.093	.106	•107	•109	•101	.084	-071	•055	•051
23	.056	.060	.081	•093	.106	.106	.108	•101	.085	.072	•057	•052
22	.057	.061	.082	• 093	.105	.105	-107	.100	•085	•073	•058	•054
21	•059	•062	.083	• 093	•104	•104	•106	.100	•085	•074	•060	•036
20	.060	.063	.084	• 093	.104	.103	.105	•100	.086	.075	.061	•057
19	.062	.065	.084	.093	.103	.102	•105	.099	.087	.076	.062	.059
18	.063	.066	.085	.093	•102	•101	•104	.099	.087	+078	•064	•060
17	.065	.067	• 686	.093	-101	+100	•103	•099	• 687	.079	+065	+062
16	•D66	.068	.086	•093	•101	•099	•102	•030	•000	.000	4007	
15	.068	.069	.087	.092	•100	•098	•101	•098	4088	.080	.068	.065
14	.069	.070	.087	.092	.009	•097	•100	•097	•088	.051	•069	•067
13	.071	.071	.088	.092	•098	• 096	•664•	.097	.088	.082	+071	• 06 8
12	.072	•072	. 689	• 092	.097	•094	•097	•096	.089	•083	• D7 Z	+070
11	+074	.073	.089	•092	.096	•093	•032	•096	•083	-004	•0/3	•0/1
10	.075	.074	.089	• 0 9 1	.095	•092	.095	•095	.089	.085	.075	+073
9	.076	.075	.090	.091	•094	•091	.094	+094	•089	: .085	-077	-075
8	.078	-076	.090	.091	+UJ4 .007	-030	•U33	1034 104	-089 -089	.087	.078	.077
7	.079	.078	.091	- 090	-092	-087	.091	.093	.089	.088	.080	.079
¢								·				
5	.082	.079	.091	•089	•091	.085	+090	•U9Z •n41	.080	,000 100	+UU1 _N#2	-000
· •	•083	.079	•U9Z	-090	4UJU 4R1	• U 0 D	-1000	1600	_0000 _089	1090	-083	.083
3	.005	•080	•052	.003	_0A7	ANA2	-086	.090	.089	.091	.085	.085
2 1	.085	•082	.092	.088	.086	.081	.085	.089	.009	.092	.086	.086
-		.047	.097	.087	.085	.080	.084	.088	.069	.092	.087	.088
	e u o 3	eyaj										

TABLE AL. POTENTIAL EVAPOTRANSPIRATION FACTOR F FOR ETP IN INCHES/NO

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500	174				MONT	- 64						
				4.00	NONI			• · · •				
	JAN	44.0	NAK	APR	HAT	JUN	JUL	AUG	SEP	OCT	NOV	DEC
-1	•090	•083	.093	.085	• 68 4	•078	•08Z	•087	•089	•093	.085	+089
-2	•091	+084	• 09 3	•086	•083	•077	•081	.086	•083	.093	.089	.091
-3	•033	.005	.093	.085	•C82	•076	.080	-046	.08.8		- 090	. 092
-4	.094	.085	-093	.085	-081	-079	.07.8	.086	-088	-004		• 11 3 2
										1034	+03T	• 033
-6	.005	0.00									_	
-3	+035	+000	•033	+004	•000	•073	4077	+054	•088	•095	•032	•095
-0	•130	•087	•0.32	•083	.078	•072	∎076	•083	.088	•095	.033	•096
-7	•098	•087	• 093	•083	•077	•070	•075	•082	.087	.096	-094	. 097
-8	•099	.088	.093	.082	.076	•069	-073	-081	-087	-096		. 099
-9	-100	.089	-093	-081	.075	-068	-072	.080	047	007	1015	•055
-									.00/	•057	+0.30	•100
-10	- 101	PA0_	. ng t	0.00	.077	Dec	070					
	100		•033	.000	•073		•010	•019	+076	•097	•097	•101
-11	• 10 2	•090	•093	•080	•07Z	•065	•069	•078	.086	•097	.098	•103
-12	-103	•090	•093	•079	+071	•063	•068	•077	.085	•098	•099	-104
-13	-104	•091	.092	•078	•07D	•062	.066	.076	.085	.098	-100	-105
-14	•106	•091	.092	.077	.068	.060	-065	-075	-084	.09.8	.101	107
											••••	
-15	.107	D92	-092	•076	-067	- 11 5 9	-063	.073	00.0	00.0		
-16	-108	.092	. 092	.075	.055	050	0003	-075	0004	+1.70	• 102	-108
-17	. 100	002	0.01		000	• 0 5 0	+062	•072	-083	•095	•103	•109
	1103	.052	-031	•074	• 064	• 0 56	•061	•071	•083	•099	.104	•110
-10	•110	•093	•0a1	+073	• 06 3	•055	•059	+070	•082	•099	•104	-111
-13	•111	•093	•091	•073	•062	•053	•058	.069	•082	.099	.105	- 173
-20	•112	•094	.090	.072	.060	.052	+056	-06A	- 081	.099	. 1 00	
-21	.113	.094	.090	.071	.059	-050	2065	-066	.040	.000	-100	+114
-22	.114	.094	-089	.070	-057	- 00	-053	-000		•023	1010	+115
-23	. 118	.004	0.00	000	1037	• 11 4 3	•053	+065	•080	•033	•107	•116
		-054	.003	• 00 3	• 855	• 0 48	•052	•054	•079	•099	.108	•117
-24	•112	•032	.088	• 067	•055	•045	•051	•063	•078	•099	•109	.118
-25	.116	•095	.088	•066	.053	• 045	.049	.062	.077	•099	-109	.119
-26	•117	.095	.087	•065	.052	.043	-048	-060	.077	.099	110	120
-27	.118	.095	.087	- 064	-050	- 042	-016	050	070	•035	•110	• 120
-28	.119	-095	.086	.063	. 05 9	040	0.5	.055	•076	•033	•111	• 121
-29	.120	.096	0.00	0003	043	•040	•1+5	•058	+U/5	.633	•111	•123
-63		+050	•000	• U 6 Z	e U 9 8	•039	-043	•056	.074	•098	•112	•124
-30	•120	•095	•085	•051	-046	•037	•092	.055	-073	.098	.113	-125
-31	•121	•096	.089	•060	•045	•036	.040	.054	.072	.098	.117	-126
-32	•122	•096	.084	.058	•043	.035	•039	-052	-071	-098	.116	. 127
-33	.123	•096	.083	.057	.042	-033	-037	-051	.070	.097		- 121
-34	.124	.096	-082	.056	.040	.032	1.DTC	.050	0000	007		+120
-			••••				1000	•U5U	•U¢3	•097	•115	•129
-15	.128		.081	0 E E	070							
-76	125	0050		.055	•123	•030	•034	•098	•1168	•097	•115	•130
- 37	• 46 7	1033	.000	•053	•037	•029	•033	+046	.067	•096	.115	•129
-31	•123	.094	•078	•051	•035	•027	+031	•044	•065	.094	.113	.129
-38	•122	.092	•076	• 049	•033	.025	•029	.042	.063	.092	.112	-128
-39	•120	•091	.074	• 047	.031	• 024	•027	.040	-061	-090	.111	.120
											****	.170
-40	•119	.089	.072	.045	.030	.022	.026	.078				
-41	-11A	-087	.070	. 043	.028	020	020	.030	•039	•088	-103	• 125
-42	.116	.080	. 000	- 043	-020	.020	P100	•037	+057	•086	•108	•124
- 11	116		-000	.041	.026	•013	•UZ Z	•°35	+C55	•085	•107	•123
	+113			• 039	• UZ 4	•017	•021	•033	.053	.083	•105	• 122
	•113	•082	.054	•037	•023	.016	•019	.031	.051	.081	.103	.120
		_ .	_									
-15	.112	.081	.062	•036	.021	•015	.018	•029	.049	.079	.102	. 110
-46	•110	•079	.059	•034	.020	.013	.016	.027	.047	.076		
-47	.108	-077	- 857	- 032	-018	.012	-015	027	-047	.010	100	+117
-18	-107	.075	.055	. 030	. 01 7	.011	4015	8U20	+645	.0/4	•038	•116
- 19	105	073	0000	.030	+UL /	•011	.013	•024	•043	•07Z	•096	•114
-43	+102	1013	• 05 3	•U28	+015	•010	•012	-022	.041	.070	+095	•112
-50	•103	.071	.051	•027	.014	•009	•011	.021	.039	.068	.093	.111
-51	.101	+069	.049	• 025	•013	.008	.010	.019	.037	nee	. 69.	
-52	• 099	.067	•047	.023	.011	.007	.009	.01.8	.016	.06+	-071	103
-53	•097	.065	.045	.022	.010	.00F	.00.	.010	-077	1 00-	•D03	• 107
-54	.095	1063	.042	.020		- 000	0000	•010	•033	.061	4086	•105
- 1						•000	•UU /	•U15	•031	•D59	.084	•103
-64		014	0 /- n					_				
-22	+U7Z	.UPI	+ 040	.019	•008	•004	•006	.013	•030	.057	.062	.101
-56	•090	•059	• 038	.017	•007	• 003	•005	.012	.D2A	.054	.080	.098
-57	.087	•057	.036	•016	.006	.003	.004	.011	.026	.052	.077	-095
-58	.085	•054	.034	.014	• CC 5	.002	.003	.010	. 02 0	.069	-075	-007
-59	•082	.052	.032	.013	.004	.002	-007	.000		0-43		
	-						-003	0003	• 02 2	•U47	•U/Z	•031
-60	.079	-UF4	-010	- 011		0.00						
				+ + + + +	PD04	+ UUL	•UÜZ	•007	•020	+044	•069	- 888
								•				

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TADLE A1. POTENTIAL EVAPOTRANSPIRATION FACTOR F FOR ETP IN INCHES PER MONTH

INDL			16 EVAF1	JIKANJE.		FACIUR	r rui					
NORT LAT	'H JAN	FCB	Mar	APR	HONTI Mây	1 Jun	JUL	AUG	SEP	001	NOV	DLC
60	.061	•177	•525	1.039	1.700	2.026	1.970	1.339	•705	•299	.089	.037
59	.077	•203	•571	1.101	1.770	2.091	1.989	1.402	.757	.334	-108	.049
58	.095	.230	.618	1.161	1.837	2.152	2.054	1.467	.809	.370	•128	.063
57	.134	• 258	• G 6 G	1.219	1.901	2.210	2.117	1.571	.861	•408	•151	+079
56	•135	•288	•714	1.277	1.962	2.265	2.176	1.592	.913	•447	•174	.097
5	•159	.319	•762	1.334	2.021	2.317	2.233	1.652	.965	-487	.200	• 116
	•103	• 352	.811	1.390	2.078	2.367	2.287	1.711	1.017	•528	•227	•138
53 57	-238	. 305	4061	1.499	2.186	2+415	2.390	1.8768	1.121	+570	•255	+15/
51	.268	.456	.961	1.552	2.238	2.506	2.439	1.879	1.172	•658	•318	•213
50	•300	.493	1.012	1.605	2.288	2.548	2.985	1.932	1.224	.703	•351	-242
19	•333	• 531	1.063	1.657	2.336	2.589	2.531	1.985	1.276	.749	.386	•272
8	•367	• 570	1.115	1.709	2.303	2.628	2.577	2.036	1.327	•796	• 422	• 304
17	.404	•610	1.167	1.760	2.429	2.665	2.616	2.086	1.379	.844	•460	• 337
16	+441	•651	1.219	1.810	2.473	2.702	2.656	2.136	1.430	•892	•499	•372
15	.481	-693	1.271	1.859	2.515	2.736	2.695	2.184	1.401	•942	•539	.409
14	•521	•736	1.324	1.908	2.557	2.769	2.733	2.231	1.532	•992	•580	+447
13	• 263	• 760	1.376	1.956	2.597	2.801	Z.769	2.277	1.583	1.042	•623	+487
	+DU/	+ 2 4	1 4 6 7	2.003	2.030	2.031	2.514	2.323	1.633	1.094	• 667	• 528
1	.031	.007	10402	2.030	2.0/4	£ • 84 U	2.031	2.367	1.084	1.145	•/12	•5/1
10	•697	•915	1.535	2.096	2.710	2.887	2.869	2.410	1.734	1.198	•758	•615
19	•744	•962	1.588	2.141	2.745	2•913	2.899	2.452	1.783	1-251	.805	• 660
<u>.</u>	•793	1.009	1.641	2.186	2.779	2.938	2.928	2.493	1+833	1.304	+854	.707
	.843	1.106	1.594	2.229	2.811	2.961	2.955	2.533	1.882	1.358	•903	• 755
•	4033	1.100	20140		20042	20303	20303	20312	1.320	1.412	• 7 2 7	.005
15 .	•940	1.148	1.789	2.301	2.856	2.987	2.991	2.596	1.967	1.458	•999	.851
54	•979	1.181	1.816	2.309	2.844	2.964	2.972	2.595	1.987	1.491	1.036	-889
3	1.018	1.214	1.842	2.317	2.832	2.941	2.953	2.595	2.006	1.524	1.073	• 929
2	1.057	1.246	1.857	2.324	2.819	2.918	2.934 2.915	2.594	2.024	1.557	1.110	.968 1.008
5	1.135	1.310	1.916	2.376	2.797	, 2 . 87 1	7.900	7 EAG	2			
9	.1.174	1.341	1.940	2.341	2.779	2.847	2.875	2.585	2.074	1.051	1.222	1.040
6	1.214	1.372	1.963	2.346	2.764	2.823	2.855	2.583	2.090	1.684	1.259	1.128
7	1.253	1.403	1.986	2.350	2.750	2.799	2.834	2.579	2.105	1.714	1.296	1.168
6	1.292	1.434	2.008	2.353	2.734	2.775	2.813	2.574	2.119	1.745	1.332	1.208
15	1.332	1.465	2.029	2.356	2.719	2.750	2.792	2.569	2.133	1.774	1.369	1.249
!	1.371	1.495	2.050	2.358	2.702	2.725	2.770	2.563	2+146	1.809	1.406	1.289
3	1.410	1.525	2.070	2.359	2.686	2.699	2.747	2.556	2.159	1.832	1.442	1.330
2	1.499	1.559	2.089	2.360	2.669	2.574	2.725	2.549	2.171	1.861	1.478	1.370
	128400	1+203	20100	2.360	2.001	2.548	2.702	2.541	2.182	1.888	1.514	1.411
20	1.527	1.612	2.126	2.359	2.633	2.621	2.678	2.533	2.192	1.916	1.550	1.451
3	1.565	1.540	2.144	2.358	2.614	2.594	2.655	2.524	2.202	1.942	1.586	1.491
7	1.607	1.606	2.101	2.356	Z+595	2.567	Z+630	2.514	2.211	1.969	1.621	1.532
6	1.680	1.723	2.193	2.353	2.575	2.540	2.5(1)	2.504	2.720	1.994 2.020	1.657	1.572
5	1.718	1.750	2.208	2.346	2-536	2.494	7.555	7.887	2.275	3 0.54	1 700	
LA	1.756	1.776	2.222	2.342	2.513	2.456	2.579	2.870	***33 7.781	2-050	1.760	1.002
3	1.794	1.802	2.236	2.337	2.491	2.427	2.503	2-457	7.747	2.092	1.795	1.772
2	1.831	1.828	2.249	2.331	2.469	2.398	2.476	2.444	2.252	2.115	1.828	1.771
11	1.868	1.853	2.261	2.324	2.447	2 . 36 9	2.449	2.430	2.256	2.137	1.862	1.811
0	1.905	1.878	2.273	2.317	2.423	7.339	2.421	2.415	2.260	2.159	1.895	1-850
9	1.941	1.902	2.284	2.310	2.400	2.309	2.393	2.400	2.263	2.120	1.928	1.849
8	1+977	1.926	2.294	2.301	2.376	7.278	2.365	2.384	2.265	2.201	1.960	1.928
7	2.013	1.949	2.303	2.292	2.351	2 - 24 7	2.336	2.368	2.267	2.221	1.192	1.906
6	2.049	1.972	2.312	2.282	2.326	2.216	2.366	7-351	2.268	2.240	2.024	2.004
5	2.084	1.994	2.320	2.272	2.300	2.185	2.277	2.733	2.268	2.259	2.055	2.043
7	2+119	2.015	2.328	2.261	2.274	7.153	2.247	2.315	2.768	2.277	2+086	2.080
2	2.188	2.050	2,240	2.277	2.248	2+121	Z.716	2.297	2.767	2.294	2.116	2.118
ī	2.272	2.074	2.346	4+631 7,774	2.101	2.055	2 . 1 Eh	24211	2.705	Z.311	2.147	2.155
						~	m = 1 27	E # E 7 I	4 + K U J	60361	Zel/6	2.192

0 2.255 2.098 2.350 2.211 2.155 2.023 2.123 2.237 2.260 2.343 2.265 2.229

TABLE AZ. POTENTIAL EVAPOTRANSPIRATION FACTOR F FOR ETP IN MH PER HOPTH

TABLE A2. POTENTIAL EVAPOTRANSPIRATION FACTOR F FOR ETP IN MM PER NONTH

										•		
501	1712				NAUTI	4						
300					nunti	nr .						
LAI	I JAN	TEB	MAR	APR	HAY	JUN	JUL	AUG	SEP	0C T	'NOV	DEC
-1	2.708	2.117	2.354	2.197	2.137	1.990	2.091	2.216	2.250	2.356	2.214	2.766
-2	2.321	2.116	2. 167	2-182	2.100	1.055	2.000	7 104	3 361			2.203
	2.157	3 1 5 4	3 360	3 17 3	2 0 70	1 000		24437	2.42.51	2.312	2.203	2.301
-3	x+333	X+134	2.00	2.0101	2.013	1.922	2.000	2.172	2.745	Z.38E	2.290	2 • 337
-4	2.305	2.172	2.362	2.151	2.050	1.888	1.993	2.150	2.240	2.398	2.318	2.372
-5	2.016	2.189	2.363	2 114	2 0 20							
-			20303	20134	24020	14034	10300	5.150	20234	2.911	2+395	2.407
-6	2.997	2.205	2.363	2.117	1.982	1.820	1.976	2.103	2.726	2.422	2.371	2.442
-7	2.470	2.221	2.363	2.099	1.959	1.785	1.893	2.078	2.218	2.431	2.197	2.476
-8	2.508	2-237	2.362	2.081	1.927	1.760	1.0.09	3 054	2 2 2 2 2 2		20337	24470
~ 0	2 674		0 300				LOUJU	2.00.54	2.210	2+443	2.423	2+510
-3	×	4+201	2+368	2.062	1.00.0	1.715	1.824	2.028	2.201	2.453	2.448	2.544
-10	2.567	2.266	2.357	2-043	1.864	1.679	1.789	2-003	2.191	2.862	7.477	3 577
-11	2.596	2.279	2.750	2 027	1 077	1 64.5		1 030		20402	20773	2.077
_ 73	0 0 0		20034	20023	1.032	1 0 0 4 4	1+1.24	7.310	2+180	2.970	2.497	• Z.61C
-12	2.023	2.292	2.350	2 • 00 2	1.799	1.608	1.713	1.950	2.169	2.477	2.520	2.643
-13	2+652	2.305	2.345	1.981	1.767	1.572	1.684	1.922	2.157	2.4 84	2-501	2.675
-14	2.680	2-317	2.340	1.959	1 . 7 17	1.676	1 6 40	1 005	3		20010	2.075
	,	20021		20333	x	1.020	1.040	1.033	2+144	2.4.30	2.560	2.705
-15	2.707	2.328	2.334	1.937	1.700	1.500	1.612	1.867	2.131	2.496	2.588	2.730
-16	2.734	2.339	2.327	1.914	1.666	1-464	1.575	1.878	2.117	2.600	2 610	2 700
-17	2.760	2. 349	2.119	1.091	1.637	1 427	1 640	1.0000		2.500	2.010	20103
	2 705	0.350	2.2223		1.032	10721	1.540	7-003	2.103	2.504	2+631	2.799
-10	2.103	5+322	2.311	1.867	7.288	1.391	1.504	1.780	2.088	2.508	2.651	2.830
-19	2.811	2.368	2.302	1.843	1.564	1.354	1.467	1.750	2.072	2.510	2.671	2.859
									2.0.2		2.0012	20033
-20	2.476		3 3 6 7									
-20	2.035	2.311	2.293	1.010	7+253	1.318	1.431	1.719	Z.056	2.512	2.691	2.889
-21	2.860	Z.385	2.282	1.792	1.494	1.281	1.394	1.689	2.039	2.514	2-710	2-918
-22	2.883	2.392	2.272	1.767	1.459	1-244	1.357	1-658	2.021	2-514	2.720	2 047
-23	2-907	2.399	2.260	1.740	1.427	1.208	1 720	1 600	2 0021	2.0344	20120	24347
- 20	2 070	2	2 2 2 2 2	10770	1.4423	1.200	10320	1.070	2+003	2.514	2.747	2.975
-24	2.0220	2.405	2 . 2 9 8	1.713	1,388	1+171	1.283	1.595	1.984	2.513	2.764	3.003
-25	2.952	2.411	2.234	1.686	1.352	1.134	1-246	1.563	1.965	7.517	2 7 8 1	7
-26	2.975	2.416	2.921	1.650	1 110	1 007		1 530	1.000	20312	20101	24031
	2.000	24410	2	1.033	1.010	1.001	1+562	1+230	1.942	Z+510	2.798	3.058
- 21	5+330	2.920	2 • • 106	1.630	1.280	1.061	1.172	1.497	1.924	2.507	2.819	3.085
-28	3.018	2.424	2.191	1.602	1.244	1.024	1.134	1.464	1.903	2.503	2.810	7.112
-29	3.039	2.427	2-176	1-573	1.208	. 99.8	1.007	1 0 71	1	2.000	20050	34112
				20010	A V L U U		1.031	10431	1.001	2.433	2.845	3.139
-30	3.059	Z•430	2.159	1+594	1.172	• 952	1.060	1.397	1.859	2.494	2.859	3-165
31	3.079	2.432	2.142	1.514	1.135	-916	1.023	1.364	1.835	2.499	2.474	7 101
-32	3.099	2.434	2.125	1.484	1.090	- 48.0	0.00		1.000	21403	2 4 0 1 4	34121
	7						• 305	1.953	1.012	2.983	2.585	3.217
-33	2.113	2.433	2.100	1.423	1.063	• 84 4	•949	1.295	1.788	2.475	2.901	3.242
-34	3.138	Z+436	2.007	1.422	1.026	.808	.912	1.261	1.764	2.469	2-914	1.268
										20105	2.0.72.4	3.500
-35	3.157	7.816	7.058	1 701	000	***						
-75	7 1	0	2 0 7 0			• 11 3	•8 /b	1.226	1.739	Z.460	2 • 927	3.293
-30	20140	2+415	2.030	1.348	•945	•731	•832	1.180	1.698	2.430	2.914	3.289
-37	3.120	2.378	1.980	1.297	•896	•686	•784	1.129	1.647	2-345	2.882	7.265
-38	3.090	2.340	1.929	1.246	.847	. 64 3	.7.18	1.077	1 507	3 7 7 6	2	54205
- 39	3.058	2.302	1.070	1 100	000	6043	• 7 30	14077	10001	2.333	2.850	3.239
- 0,	31030	24 302	1+010	74730	• 8 00	• 60 U	• 6 92	1.027	1.546	2.293	2.816	3.212
												-
-40	3.025	2.262	1.826	1.146	.753	• 55 9	-640	-977	1.495	2.245	3 740	~
-41	2.991	2.222	1.774	1.096	.708	. E1 9'	C 0C	000		2.243	2.0700	2.102
-12	2.955	2 4 80	1 700	10000			• 61.3	. 328	1.4444	2.197	2+744	3.153
	20000	2.100	1.122	1.0047	• 564	• 480	•563	•850	1.393	2.147	2.706	3.122
-43	2.918	2.138	1.659	• 9 9 9	•620	• 44 3	•572	.832	1.343	2.097	2.666	3-080
-44	2.879	2.095	1.617	.951	•578	- 407	- 8 83	-786	1.202	2.047	2 6 2 6	3 053
•							0105		102 32	20097	2.020	2-022
-15	2.819	2.050	1 564	00.0	<i>~</i>	-						
		24055	1.004		•23/	•372	• 4 4 5	•740	1.241	1.995	2.584	3.017
	2.797	2.005	1.510	-857	•498	• 339	• 408	.696	1.191	1.967	2.540	7 070
-47	2.754	1.959	1.457	.811	.459	- 307	. 371				2.0340	20313
- 88	2.709	1-912	1-403	766	4.20			1052	T . T . T	1.030	2.435	2.939
	2.667	1	1 100	1700	****	• 21 0	• 2 2 3	+609	1.091	1.836	2.450	2.098
-43	¥+003	74004	1.920	• 721	•387	• 24 7	•307	•567	1.041	1.781	2.402	2.855
											20102	24035
-50	2.615	1.814	1.296	.677	-352	. 220	. 976	8 4 H				
-51	2.565	1.768	1.242	694			• 6 / 0	•72T	•275	1+725	Z•353	Z.810
	2 E 4 7	4 74 4	*****	• • • • • •	•212	•199	•245	-487	-943	1.670	2.302	2.763
-96	6+013	10/13	10100	• 59Z	•288	+170	.218	•449	.894	1.613	2.250	2.716
-23	Z+459	1.661	1.133	•551	•258	.147	.192			. 1.666	7.100	2 6 6 4 2
-54	2.403	1.607	1.079	.511	.229	-176	. 1	774			24130	2.004
- •						4 4 4 9	01L0	• 376	•797	1.997	2.140	2.611
- **												-
-22	2.545	1.52	1.025	•471	-202	•106	•144	.341	.750	1.418	2.082	2.85E
-56	Z.285	1.496	.970	.433	.176	-088	.121	. 30.0	. 7 . 7		A 002	
-57	2.221	1.438	.916	396	.141		107	-300	• • • • • •	1+377	2.072	2 • 4 9 8
-54	2.166	1.170		360	1	• • • • •	•103	+275	• 556	1.316	1.959	2.437
- 50		4.310	*001	4 36 U	•1 30	•057	.085	•246	.610	1.253	1.894	2-374
-22	2.085	1.317	•806	• 325	•110	•045	.069	-217	- 564	1.1.40	1.196	2.707
						- • •				44407	T#010	2 0 J U I
-60	2.012	1.253	.751	. 781	.091		Ar-		_			
				**3*	eu 31	•033	•U55	e169	•519	1.124	1.755	2.236

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